

Designer's casebook

during the cycle to trigger Q_2 .

Now that C_2 has been determined, C_1 can be found.

$$C_1 = C_2/21 = 0.025 \times 10^{-6}/21 \\ = 0.0012 \text{ microfarads.}$$

The circuit was constructed using the components determined above and performed reliably from 0° to 65°C .

Constant-current source controls sweep rate

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A constant-current generator stage is used in this circuit to obtain linear sweeps ranging from a few microseconds to one second in duration. The constant-current source portion of the circuit, contained within the dashed-line box, consists of Q_2 , R_3 , R_4 , and R_5 .

Transistor Q_2 , in the constant-current source stage, and transistors Q_3 and Q_4 , which are connected in a Darlington amplifier configuration, conduct at all times during the operation of the circuit.

At first, an input voltage $-E_i$ is applied to the base of the emitter-follower Q_1 . This voltage maintains Q_1 in conduction, and places nearly $-E_i$ volts at the upper plate of capacitor C through a path consisting of R_2 and D_1 .

When the input signal rises to ground, Q_1 is cut off; diode D_1 becomes back biased and also stops conducting.

Now the only current being supplied to the capacitor is the small positive current from the constant-current source. The voltage across C increases linearly from approximately $-E_i$ volts and approaches $+V_{ce}$, the voltage at the collector of Q_2 . This process continues until the input pulse is removed—before or when the voltage at the upper plate of C reaches ground potential.

With the return of the input signal to $-E_i$ volts, Q_1 and D_1 conduct, and the upper plate of the capacitor also goes to $-E_i$ volts.

The voltage across a capacitor is defined by:

$$V_C = 1/C \int i dt$$

With a constant current flowing, this becomes:

$$V_C = (i)(t)/C$$

In a typical application, with an input pulse voltage ($-E_i$) of -12 volts, the constant-current source was set at two milliamperes. The total sweep time desired was 100 microseconds, and a full 12-volt sweep was also desired. Therefore:

$$C = (2 \times 10^{-3})(10^{-4})/12 \\ = 0.016 \text{ microfarad}$$

The retrace time T_R (time for the voltage to revert to nearly $-E_i$) is given by:

$$T_R = 3 RC$$

where

$$R = (Z_S/\beta_1) + Z_{D1} + R_2$$

$$\beta_1 = \text{Beta of } Q_1$$

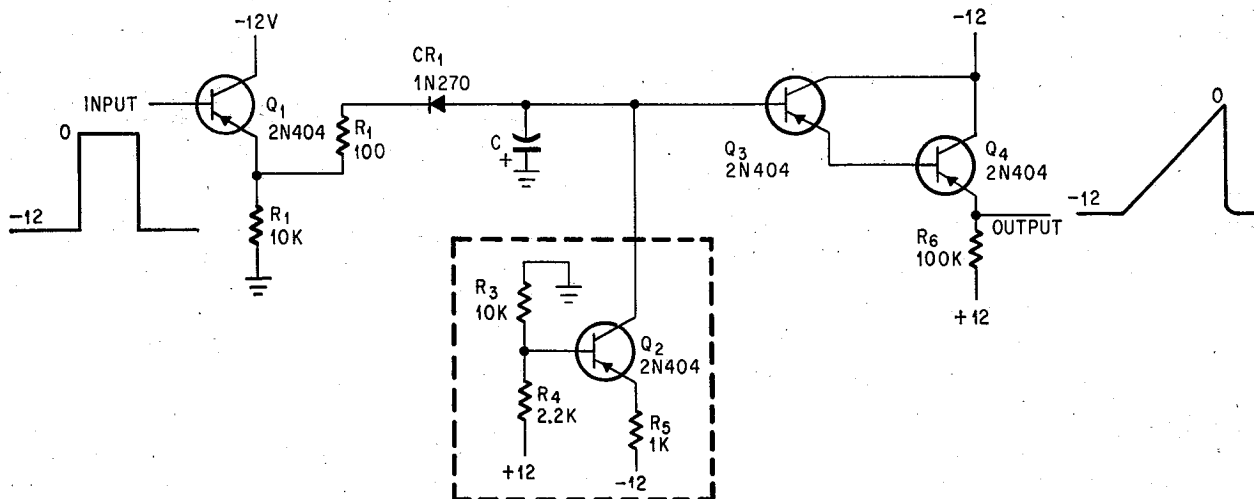
$$Z_S = \text{Source impedance}$$

$$Z_{D1} = \text{Forward impedance of } D_1$$

For the example specified above, the retrace time was about four microseconds.

The Darlington connection of Q_3 and Q_4 presents a high input impedance to the sweep circuit and acts as a buffer to the load. For sweep times greater than one second, with good linearity, Q_3 should be replaced with a transistor having high current gain with low base current.

Resistor R_2 was added to the circuit to limit the peak current handled by Q_1 during the discharge of C . Resistor R_2 is 100 ohms.



The constant-current generator stage (shown in dashed box) supplies a 2-milliamper current to the capacitor.